Richard Nakka's Experimental Rocketry Web Site

Technical Notepad #5 -- KNER Ideal Performance Calculations

Note 1

Potassium Nitrate - Erythritol (KNER) propellant

65/35 O/F ratio @ 1000 psia chamber pressure

From PROPEP results, for 100 grams mixture:

KNER Run using June 1988 Version of PEP, Case 1 of 1 29 Nov 2006 at 8:48: 8.54 pm									
CODE WEIGHT D-H DENS COMPOSITION 821 POTASSIUM NITRATE 65.000 -1169 0.07620 1N 30 1K 1091 ERYTHRITOL 35.000 -1731 0.05240 4C 10H 40									
THE PROPELLANT DENSITY IS 0.06575 LB/CU-IN OR 1.8199 GM/CC THE TOTAL PROPELLANT WEIGHT IS 100.0000 GRAMS									
NUMBER OF GRAM ATOMS OF EACH ELEMENT PRESENT IN INGREDIENTS									
2.865940 H 1.146376 C 0.642877 N 3.075006 O 0.642877 K									

T(K) T(F) P(ATM) P(PSI) ENTHALPY ENTROPY CP/CV GAS RT/V 1608. 2435. 68.02 1000.00 -136.57 172.02 1.1392 2.593 26.237									
SPECIFIC HEAT (MOLAR) OF GAS AND TOTAL= 10.214 14.503 NUMBER MOLS GAS AND CONDENSED= 2.5927 0.3147									
0.95381 H2O									
THE MOLECULAR WEIGHT OF THE MIXTURE IS 34.395									

T(K) T(F) P(ATM) P(PSI) ENTHALPY ENTROPY CP/CV GAS RT/V 1030. 1394. 1.00 14.70 -164.52 172.02 1.1518 2.579 0.388									
SPECIFIC HEAT (MOLAR) OF GAS AND TOTAL= 9.367 13.407 NUMBER MOLS GAS AND CONDENSED= 2.5787 0.3214									
0.78506 H2O									
THE MOLECULAR WEIGHT OF THE MIXTURE IS 34.481									
********PERFORMANCE: FROZEN ON FIRST LINE, SHIFTING ON SECOND LINE*******									
IMPULSE IS EX T* P* C* ISP* OPT-EX D-ISP A*M EX-T 153.8 1.1451 1499. 39.14 3024.7 9.94 279.9 0.09403 942.									
156.0 1.1145 1523. 39.57 3089.1 116.9 10.43 283.8 0.09603 1030.									

The effective Molecular Weight is given by dividing the number GAS moles into the system mass. Since the system mass is 100 grams:

$$MW(effective) = \frac{100}{2.5787} = 38.78 \text{ g/mole}$$

Note that this is the proper molecular weight to use in the thermodynamic equations.

The mass fraction of condensed phase is given by the mass of the condensed phase (K_2CO_3) divided by the system mass

The MW of
$$K_2CO_3$$
 = 138.21 g/mole, thus
$$X = \frac{0.3214 \left(138.21\right)}{100} = 0.444$$

Note 2

KNER 65/35 O/F ratio @ 1000 psia chamber pressure

Mole fractions and mass fractions for each combustion product are calculated in the table below:

		MW	Number	Mole	System	Mass
		(g/mol)	of moles	fraction	mass (g)	fraction
	CO	28.01	0.4991	0.1717	13.978	0.1398
	H2	2.02	0.4722	0.1624	0.954	0.0095
	KH	40.11	0.0000	0.0000	0.000	0.0000
	N2	28.02	0.3213	0.1105	9.003	0.0900
	CO2	44.01	0.3325	0.1144	14.635	0.1464
	H2O	18.02	0.9538	0.3281	17.188	0.1719
	KOH	56.11	0.0129	0.0044	0.721	0.0072
	ОН	17.01	0.0000	0.0000	0.000	0.0000
	Н	1.01	0.0000	0.0000	0.000	0.0000
	K	39.1	0.0005	0.0002	0.020	0.0002
	K202H2	112.22	0.0001	0.0000	0.008	0.0001
	K2C03(L)	138.21	0.3147	0.1082	43,491	0.4349
	total moles:		2.9070	1.000	100.00	1.000
	ga	is moles:	2.5924	0.8918	56.508	0.5651
cond	ensed phas	e moles:	0.3147	0.1082	43,491	0.4349

The table below shows the computation of k, the ratio of specific heats:

	Specific Heat of solid (Cs) and gas (Cp) at constant pressure											
	Cs Cp											
Temp	K₂CO₃	KOH	CO	CO ₂	H ₂	H₂O	N ₂	Gas	Mixture	k	k'	k
K	Ref. JANAF	Ref. NIST		F	Ref. JANAF			only		mixture	gas	2-phase
300	114.70		29.14	37.221	28.849	33.60	29.125	31.62	45.54	1.2233	1.3568	1.0745
400	128.14		29.34	41.325	29.181	34.26	29.249	32.50	48.06	1.2092	1.3437	1.0677
500	140.05		29.75	44.627	29.26	35.23	29.58	33.42	50.42	1.1975	1.3312	1.0626
600	150.67		30.44	47.321	29.327	36.33	30.11	34.38	52.67	1.1874	1.3190	1.0585
700	160.48		31.17	49.564	29.441	37.50	30.754	35.34	54.82	1.1788	1.3077	1.0552
800	170.04		31.90	51.434	29.624	38.72	31.433	36.29	56.93	1.1710	1.2972	1.0523
900	179.52		32.58	52.999	29.881	39.99	32.09	37.21	59.01	1.1640	1.2877	1.0498
1000	188.95		33.18	54.308	30.205	41.27	32.697	38.10	61.04	1.1577	1.2791	1.0474
1100	198.32		33.71	55.409	30.581	42.54	33.241	38.95	63.03	1.1520	1.2714	1.0454
1200	205.26		34.18	56.342	30.992	43.77	33.723	39.74	64.67	1.1475	1.2645	1.0439
1300	209.20		34.57	57.137	31.423	44.95	34.147	40.49	65.89	1.1444	1.2584	1.0430
1400	209.20		34.92	57.802	31.861	46.05	34.518	41.17	66.57	1.1427	1.2530	1.0429
1500	209.20		35.22	58.379	32.298	47.09	34.843	41.81	67.20	1.1412	1.2483	1.0427
1600	209.20	57.5	35.48	58.886	32.725	48.05	35.128	42.67	68.07	1.1391	1.2420	1.0426
1700	209.20	57.8	35.71	59.317	32.139	48.94	35.378	43.02	68.42	1.1383	1.2395	1.0425
1800	209.20	58.1	35.91	59.701	33.537	49.75	35.6	43.69	69.09	1.1368	1.2350	1.0423
1900	209.20	58.4	36.09	60.049	33.917	50.50	35.796	44.14	69.54	1.1358	1.2321	1.0422
2000	209.20	58.7	36.25	60.35	34.28	51.18	35.971	44.55	69.95	1.1349	1.2294	1.0421
2100	209.20	58.9	36.39	60.622	34.624	51.82	36.126	44.94	70.34	1.1341	1.2270	1.0421
2200	209.20	59.1	36.52	60.865	34.952	52.41	36.268	45.29	70.69	1.1333	1.2249	1.0420
2300	209.20		36.64	61.086	35.263	52.95	36.395	45.31	70.71	1.1332	1.2247	1.0420
2400	209.20		36.32	61.287	35.559	53.44	36.511	45.53	70.93	1.1328	1.2234	1.0419
2500	209.20		36.84	61.471	35.842	53.90	36.616	45.89	71.29	1.1320	1.2213	1.0419
	Note: Units of Cp and Cs are J/mol-K											

The values for Cp and Cs are taken from the JANAF Thermochemical Tables and NIST Chemistry WebBook.

Note that the highlighted range (yellow) is applicable for interpolation of the values at 1608 K, the chamber combustion temperature under consideration.

The Cp for the gas only products and mixture (gas+condensed) is given by

$$\begin{split} Cp_{\text{gas}} &= \frac{1}{n} \sum_{i} \; n_{i} \; Cp_{i} \\ Cp_{\text{mix}} &= \frac{1}{n} \sum_{i} \; \left(n_{i} \; Cp_{i} + n_{s} \; C_{s} \right) \end{split}$$

where n_i is the number of moles of gas component i, n_s the number of moles of condensed component, n the total number of gas moles. The ratio of specific heats for the mixture, for the gas-only, and for two-phase flow is given by

$$\mathbf{k}_{\text{mix}} = \frac{\mathbf{C}\mathbf{p}_{\text{mix}}}{\mathbf{C}\mathbf{p}_{\text{mix}} - \overline{\mathbf{R}}}$$
 where $\overline{\mathbf{R}} = 8.314$ J/mol-K (universal gas constant).
$$\mathbf{k}'_{\text{(gas)}} = \frac{\mathbf{C}\mathbf{p}_{\text{gas}}}{\mathbf{C}\mathbf{p}_{\text{gas}} - \overline{\mathbf{R}}}$$

$$\mathbf{k}_{2ph} = \mathbf{k'} \left[\frac{1 + \psi \frac{Cs}{Cp_{gas}}}{1 + \mathbf{k'} \psi \frac{Cs}{Cp_{gas}}} \right]$$

where $\psi = X/(1-X)$.

Note that k for two-phase (gas+condensed) flow is a modified form of the gas-only k'. This is the correct form of k to use in the thermodynamic equations involving products with a significant fraction of condensed-phase particles. The value of k given in the PROPEP output (Cp/Cv) is for the mixture.

Note 3

Characteristic exhaust velocity is given by

$$c^{\star} = \sqrt{\frac{\overline{R}\,T_{\text{o}}}{M\,\,k}} \left(\frac{k+1}{2}\right)^{\frac{k+1}{k-1}}$$

with

To = 1608 K

M = 38.78 kg/kmol

k = 1.1390 Note: k for the *mixture* is the proper value to use, as c* represents a static condition $\bar{\mathbb{R}}$ = 8314 J/kmol-K

this gives $c^* = 923 \text{ m/s} (3027 \text{ ft/s}).$

Note 4

The propellant specific impulse is given by the effective exhaust velocity divided by g.

$$\mathrm{Isp} = \ \frac{c}{g} = \frac{1}{g} \sqrt{\frac{2\,k}{\left(k-1\right)} \, \frac{\overline{R} \, T_o}{M}} \left[1 - \left(\frac{P_e}{P_o}\right)^{\frac{k-1}{k}}\right]$$

with

To = 1608 K

M = 38.78 kg/kmol

k = 1.0426 Note: k for 2-phase flow is the proper value to use, as *Isp* involves two-phase flow.

Thus, Isp = 167 sec.

for standard conditions of Po = 68 atm. (1000 psia) and Pe = 1 atm., and g = 9.806 m/s (maximum theoretical, assumes frozen equilibrium, and no particle velocity lag or thermal lag).

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