# Richard Nakka's Experimental Rocketry Web Site 

## Technical Notepad \#5 -- KNER Ideal Performance Calculations

Note 1
Potassium Nitrate - Erythritol (KNER) propellant
65/35 O/F ratio @ 1000 psia chamber pressure
From PROPEP results, for 100 grams mixture:


THE PROPELLANT DENSITY IS $0.06575 \mathrm{LB} / \mathrm{CU}-\mathrm{IN}$ OR $1.8199 \mathrm{GM} / \mathrm{CC}$ THE TOTAL PROPELLANT WEIGHT IS 100.0000 GRAMS

NUMBER OF GRAM ATOMS OF EACH ELEMENT PRESENT IN INGREDIENTS

| 2.865940 H | 1.146376 C | 0.642877 N | 3.0750060 |
| :--- | :--- | :--- | :--- | :--- |
| 0.642877 K |  |  |  |



THE MOLECULAR WEIGHT OF THE MIXTURE IS 34.481

| IMPULSE | IS EX | T* | P* | $C^{*}$ | ISP* | OPT-EX | D-ISP | A*M | EX-T |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 153.8 | 1.1451 | 1499. | 39.14 | 3024.7 |  | 9.94 | 279.9 | 0.09403 | 942. |
| 156.0 | 1.1145 | 1523. | 39.57 | 3089.1 | 116.9 | 10.43 | 283.8 | 0.09603 | 1030. |

The effective Molecular Weight is given by dividing the number GAS moles into the system mass. Since the system mass is 100 grams:
$\mathrm{MW}($ effective $)=\frac{100}{2.5787}=38.78 \mathrm{~g} / \mathrm{mole}$

Note that this is the proper molecular weight to use in the thermodynamic equations.
The mass fraction of condensed phase is given by the mass of the condensed phase $\left(\mathrm{K}_{2} \mathrm{CO}_{3}\right)$ divided by the system mass

The MW of $\mathrm{K}_{2} \mathrm{CO}_{3}=138.21 \mathrm{~g} / \mathrm{mole}$, thus

$$
x=\frac{0.3214(138.21)}{100}=0.444
$$

Note 2
KNER 65/35 O/F ratio @ 1000 psia chamber pressure

Mole fractions and mass fractions for each combustion product are calculated in the table below:

|  | $\begin{gathered} \mathrm{MW} \\ (\mathrm{~g} / \mathrm{mol}) \end{gathered}$ | Number of moles | Mole fraction | System mass (g) | Mass fraction |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CO | 28.01 | 0.4991 | 0.1717 | 13.978 | 0.1398 |
| H2 | 2.02 | 0.4722 | 0.1624 | 0.954 | 0.0095 |
| KH | 40.11 | 0.0000 | 0.0000 | 0.000 | 0.0100 |
| N2 | 28.02 | 0.3213 | 0.1105 | 9.003 | 0.09010 |
| CO 2 | 44.01 | 0.3325 | 0.1144 | 14.635 | 0.1464 |
| H2O | 18.02 | 0.9538 | 0.3281 | 17.188 | 0.1719 |
| KOH | 56.11 | 0.0129 | 0.0044 | 0.721 | 0.0072 |
| OH | 17.01 | 0.0000 | 0.0000 | 0.000 | 0.0100 |
| H | 1.01 | 0.0000 | 0.0000 | 0.000 | 0.0100 |
| K | 39.1 | 0.0005 | 0.0002 | 0.020 | 0.0002 |
| K2O2H2 | 112.22 | 0.0001 | 0.0000 | 0.008 | 0.0001 |
| K2C03(L) | 138.21 | 0.3147 | 0.1082 | 43.491 | 0.4349 |
| total moles: gas moles: ensed phase moles: |  | 2.9070 | 1.000 | 100.00 | 1.000 |
|  |  | 2.5924 | 0.8918 | 56.5018 | 0.5651 |
|  |  | 0.3147 | 0.1082 | 43.491 | 0.4349 |

The table below shows the computation of $\boldsymbol{k}$, the ratio of specific heats:

|  | Specific Heat of solid (Cs) and gas (Cp) at constant pressure |  |  |  |  |  |  |  |  | k mixture | $\begin{gathered} \mathbf{k}^{\prime} \\ \text { gas } \end{gathered}$ | $\begin{array}{\|c\|} \hline \mathbf{k} \\ \text { 2-phase } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cs | Cp |  |  |  |  |  |  |  |  |  |  |
| Temp | $\mathrm{K}_{2} \mathrm{CO}_{3}$ | KOH | CO | $\mathrm{CO}_{2}$ | $\mathrm{H}_{2}$ | $\mathrm{H}_{2} \mathrm{O}$ | $\mathrm{N}_{2}$ | Gas <br> only | Mixture |  |  |  |
| K | Ref. JANAF | Ref. NIST | Ref. JANAF |  |  |  |  |  |  |  |  |  |
| 300 | 114.70 |  | 29.14 | 37.221 | 28.849 | 33.60 | 29.125 | 31.62 | 45.54 | 1.2233 | 1.3568 | 1.0745 |
| 400 | 128.14 |  | 29.34 | 41.325 | 29.181 | 34.26 | 29.249 | 32.50 | 48.06 | 1.2092 | 1.3437 | 1.0677 |
| 500 | 140.05 |  | 29.75 | 44.627 | 29.26 | 35.23 | 29.58 | 33.42 | 50.42 | 1.1975 | 1.3312 | 1.0626 |
| 600 | 150.67 |  | 30.44 | 47.321 | 29.327 | 36.33 | 30.11 | 34.38 | 52.67 | 1.1874 | 1.3190 | 1.0585 |
| 700 | 160.48 |  | 31.17 | 49.564 | 29.441 | 37.50 | 30.754 | 35.34 | 54.82 | 1.1788 | 1.3077 | 1.0552 |
| 800 | 170.04 |  | 31.90 | 51.434 | 29.624 | 38.72 | 31.433 | 36.29 | 56.93 | 1.1710 | 1.2972 | 1.0523 |
| 900 | 179.52 |  | 32.58 | 52.999 | 29.881 | 39.99 | 32.09 | 37.21 | 59.01 | 1.1640 | 1.2877 | 1.0498 |
| 1000 | 188.95 |  | 33.18 | 54.308 | 30.205 | 41.27 | 32.697 | 38.10 | 61.04 | 1.1577 | 1.2791 | 1.0474 |
| 1100 | 198.32 |  | 33.71 | 55.409 | 30.581 | 42.54 | 33.241 | 38.95 | 63.03 | 1.1520 | 1.2714 | 1.0454 |
| 1200 | 205.26 |  | 34.18 | 56.342 | 30.992 | 43.77 | 33.723 | 39.74 | 64.67 | 1.1475 | 1.2645 | 1.0439 |
| 1300 | 209.20 |  | 34.57 | 57.137 | 31.423 | 44.95 | 34.147 | 40.49 | 65.89 | 1.1444 | 1.2584 | 1.0430 |
| 1400 | 209.20 |  | 34.92 | 57.802 | 31.861 | 46.05 | 34.518 | 41.17 | 66.57 | 1.1427 | 1.2530 | 1.0429 |
| 1500 | 209.20 |  | 35.22 | 58.379 | 32.298 | 47.09 | 34.843 | 41.81 | 67.20 | 1.1412 | 1.2483 | 1.0427 |
| 1600 | 209.20 | 57.5 | 35.48 | 58.886 | 32.725 | 48.05 | 35.128 | 42.67 | 68.07 | 1.1391 | 1.2420 | 1.0426 |
| 1700 | 209.20 | 57.8 | 35.71 | 59.317 | 32.139 | 48.94 | 35.378 | 43.02 | 68.42 | 1.1383 | 1.2395 | 1.0425 |
| 1800 | 209.20 | 58.1 | 35.91 | 59.701 | 33.537 | 49.75 | 35.6 | 43.69 | 69.09 | 1.1368 | 1.2350 | 1.0423 |
| 1900 | 209.20 | 58.4 | 36.09 | 60.049 | 33.917 | 50.50 | 35.796 | 44.14 | 69.54 | 1.1358 | 1.2321 | 1.0422 |
| 2000 | 209.20 | 58.7 | 36.25 | 60.35 | 34.28 | 51.18 | 35.971 | 44.55 | 69.95 | 1.1349 | 1.2294 | 1.0421 |
| 2100 | 209.20 | 58.9 | 36.39 | 60.622 | 34.624 | 51.82 | 36.126 | 44.94 | 70.34 | 1.1341 | 1.2270 | 1.0421 |
| 2200 | 209.20 | 59.1 | 36.52 | 60.865 | 34.952 | 52.41 | 36.268 | 45.29 | 70.69 | 1.1333 | 1.2249 | 1.0420 |
| 2300 | 209.20 |  | 36.64 | 61.086 | 35.263 | 52.95 | 36.395 | 45.31 | 70.71 | 1.1332 | 1.2247 | 1.0420 |
| 2400 | 209.20 |  | 36.32 | 61.287 | 35.559 | 53.44 | 36.511 | 45.53 | 70.93 | 1.1328 | 1.2234 | 1.0419 |
| 2500 | 209.20 |  | 36.84 | 61.471 | 35.842 | 53.90 | 36.616 | 45.89 | 71.29 | 1.1320 | 1.2213 | 1.0419 |
|  | Note: Units of Cp and Cs are J/mol-K |  |  |  |  |  |  |  |  |  |  |  |

The values for Cp and Cs are taken from the JANAF Thermochemical Tables and NIST Chemistry WebBook.
Note that the highlighted range (yellow) is applicable for interpolation of the values at 1608 K , the chamber combustion temperature under consideration.

The Cp for the gas only products and mixture (gas+condensed) is given by
$\mathrm{Cp}_{\mathrm{gas}}=\frac{1}{\mathrm{n}} \sum_{\mathrm{i}} \mathrm{n}_{\mathrm{i}} \mathrm{Cp}$
$\mathrm{Cp}_{\text {mix }}=\frac{1}{\mathrm{n}} \sum_{\mathrm{i}}\left(\mathrm{n}_{\mathrm{i}} \mathrm{Cp}_{\mathrm{i}}+\mathrm{n}_{\mathrm{s}} \mathrm{C}_{\mathrm{s}}\right)$
where $n_{i}$ is the number of moles of gas component $i, n_{s}$ the number of moles of condensed component, $n$ the total number of gas moles. The ratio of specific heats for the mixture, for the gas-only, and for two-phase flow is given by
$\begin{aligned} \mathrm{k}_{\text {mix }} & =\frac{C p_{\text {mix }}}{C p_{\text {mix }}-\overline{\mathrm{R}}} \quad \text { where } \overline{\mathrm{R}}=8.314 \mathrm{~J} / \mathrm{mol}-\mathrm{K} \text { (universal gas constant). } \\ \mathrm{k}_{\text {(gas) }}^{\prime} & =\frac{C p_{\text {gas }}}{C p_{\text {gas }}-\overline{\mathrm{R}}}\end{aligned}$
$k_{2 p h}=k^{\prime}\left[\frac{1+\psi \frac{C s}{C p_{\text {gas }}}}{1+k^{\prime} \psi \frac{C s}{C p_{\text {gas }}}}\right]$
where $\psi=X /(1-X)$.

Note that $k$ for two-phase (gas+condensed) flow is a modified form of the gas-only $k^{\prime}$. This is the correct form of $k$ to use in the thermodynamic equations involving products with a significant fraction of condensed-phase particles. The value of $k$ given in the PROPEP output $(\mathrm{Cp} / \mathrm{Cv})$ is for the mixture.

## Note 3

Characteristic exhaust velocity is given by
$c^{\star}=\sqrt{\frac{\bar{R} T_{0}}{M k}\left(\frac{k+1}{2}\right)^{\frac{k+1}{k-1}}}$
with
To $=1608 \mathrm{~K}$
$\mathrm{M}=38.78 \mathrm{~kg} / \mathrm{kmol}$
$\mathrm{k}=1.1390 \quad$ Note: k for the mixture is the proper value to use, as $\mathrm{c}^{*}$ represents a static condition
$\overline{\mathrm{R}}=8314 \mathrm{~J} / \mathrm{kmol}-\mathrm{K}$
this gives $\mathrm{c}^{*}=923 \mathrm{~m} / \mathrm{s}(3027 \mathrm{ft} / \mathrm{s})$.
Note 4

The propellant specific impulse is given by the effective exhaust velocity divided by g .
$I_{s p}=\frac{c}{g}=\frac{1}{g} \sqrt{\frac{2 k}{(k-1)} \frac{\bar{R} T_{0}}{M}\left[1-\left(\frac{P_{e}}{P_{0}}\right)^{\frac{k-1}{k}}\right]}$
with
To $=1608 \mathrm{~K}$
$\mathrm{M}=38.78 \mathrm{~kg} / \mathrm{kmol}$
$\mathrm{k}=1.0426 \quad$ Note: k for 2-phase flow is the proper value to use, as $I s p$ involves two-phase flow.
Thus, $I s p=167 \mathrm{sec}$.
for standard conditions of $\mathrm{Po}=68 \mathrm{~atm}$. ( 1000 psia ) and $\mathrm{Pe}=1 \mathrm{~atm} .$, and $\mathrm{g}=9.806 \mathrm{~m} / \mathrm{s}$
(maximum theoretical, assumes frozen equilibrium, and no particle velocity lag or thermal lag).

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